



# Correcting Detector Plane Misalignment with Projective Geometry

8th Annual Loma Linda Algorithm Workshop

Kirk Duffin, Nicholas Karonis, Caesar Ordoñez, John Winans,  
Fritz DeJongh, Ethan DeJongh



Northern Illinois  
University

ProtonVDA

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# PROJECTIVE GEOMETRY - HISTORY



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- 19th century - organize geometry - Felix Klein - Erlangen program



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- 2 lines always intersect, parallel lines intersect at infinity

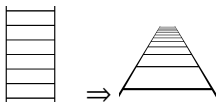
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- parallel lines not preserved

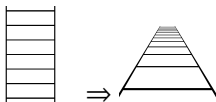


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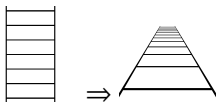
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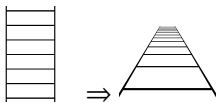
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- parallel lines not preserved
- distance not preserved
- angles not preserved
- no circles, but conic(s)

# PROJECTIVE TRANSFORMATIONS

In  $n$  dimensions there exists a projective transformation to take any arbitrary (non-collinear)  $(n + 2)$  points (projective frame) to any other arbitrary projective frame.

# HOMOGENEOUS COORDINATES

- $n$  dimensional point represented by  $n + 1$  coordinate values.  
2D —  $[x \ y \ w]$ .

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$$[3 \ 2 \ 1]$$

$$[6 \ 4 \ 2]$$

$$[0.3 \ 0.2 \ 0.2]$$

$$[30 \ 20 \ 10]$$

all represent the same point



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- Cartesian to homogenous conversion

$$(x, y) \Rightarrow [x \ y \ 1]$$

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- Cartesian to homogenous conversion

$$(x, y) \Rightarrow [x \ y \ 1]$$

- Homogeneous to cartesian conversion (normalization)

$$[x \ y \ w] \Rightarrow (x/w, y/w)$$

- Point at infinity has  $w = 0$ .



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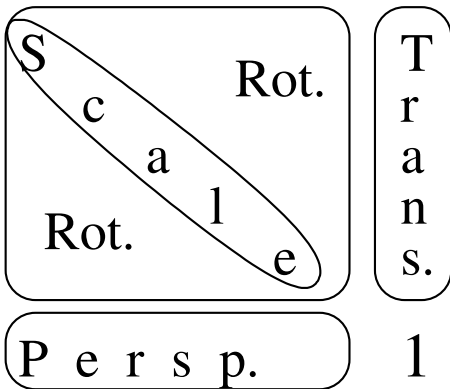
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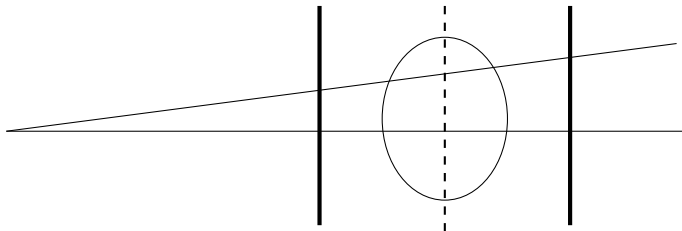
- In  $n$  dimensions,  $(n + 1) \times (n + 1)$  linear transformation matrix
- Unique up to a scale factor
- Includes standard affine transformations — translation, scale, rotation. Adds perspective transformations.
- Transformation composition through matrix multiplication

# PROJECTIVE TRANSFORMATIONS



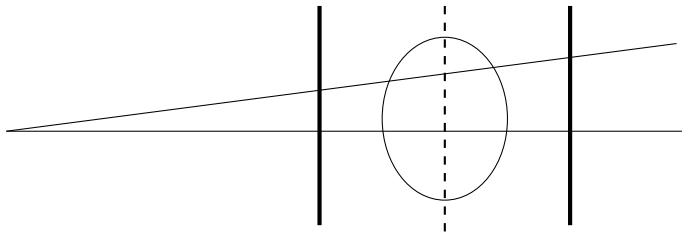


## PCT



Assumptions:

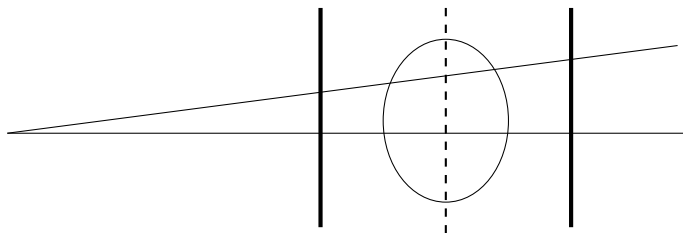
## PCT



Assumptions:

- Detector planes perpendicular to beam axis

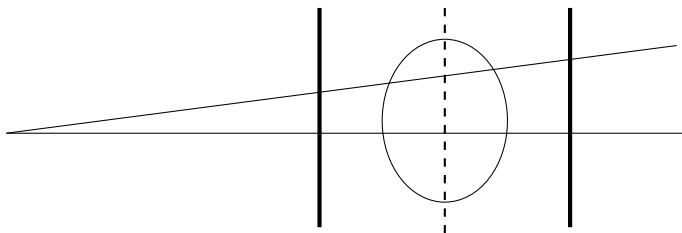
## pCT



Assumptions:

- Detector planes perpendicular to beam axis
- Distance of detector planes from isocenter

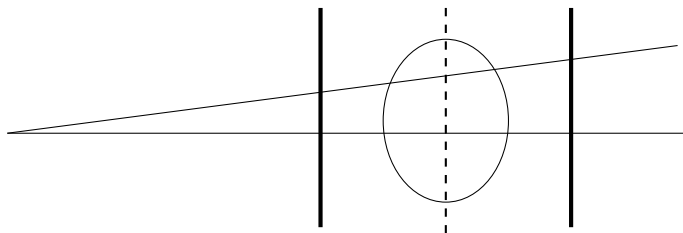
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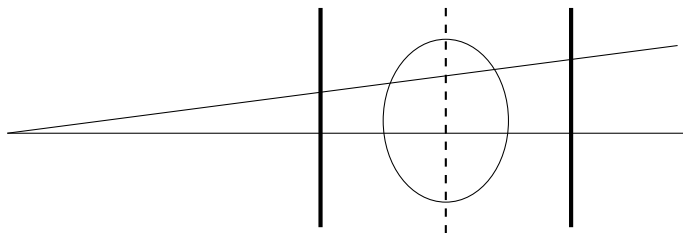
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- Distance of detector planes from beam vergence point
- Detector construction



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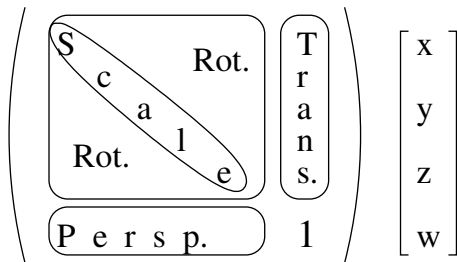
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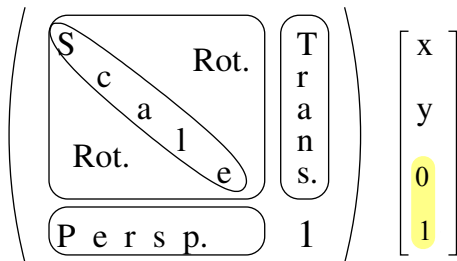
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- Idea 2: Go to 2D
- Idea 3: Directly determine final transformation matrix

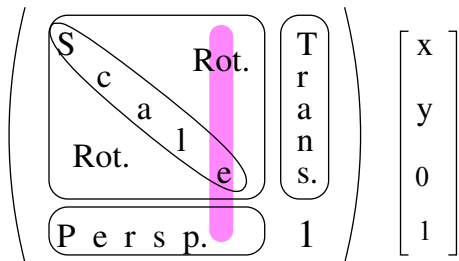
## 2D TRANSFORMATION SUFFICES



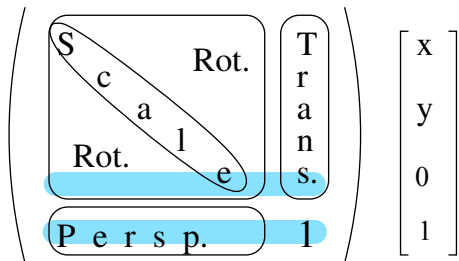
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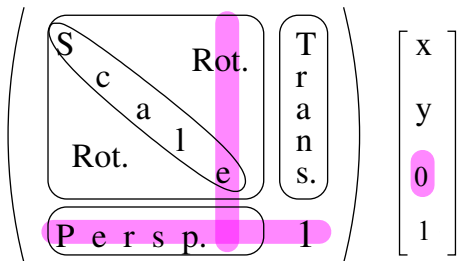




## 2D TRANSFORMATION SUFFICES

$$\left( \begin{array}{c} \text{S c a l e} \\ \text{R o t.} \\ \text{P e r s p.} \end{array} \right) \left( \begin{array}{c} \text{R o t.} \\ \text{T r a n s.} \\ 1 \end{array} \right) \begin{bmatrix} x \\ y \\ 0 \\ 1 \end{bmatrix}$$

## 2D TRANSFORMATION SUFFICES



## SOLVING FOR THE MATRIX

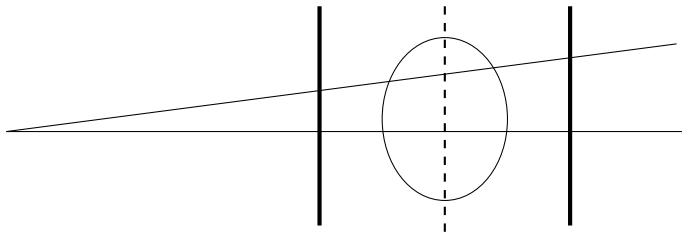
Goal: Find 2D (3x3) projective transformation matrix  $M$  that will transform a measured point  $p_m$  on a detector into the coordinates of a point  $p_i$  on the ideal detector plane.

$$p_i = Mp_m, \begin{pmatrix} x_i \\ y_i \\ w_i \end{pmatrix} = \begin{pmatrix} m_{00} & m_{01} & m_{02} \\ m_{10} & m_{11} & m_{12} \\ m_{20} & m_{21} & 1 \end{pmatrix} \begin{pmatrix} x_m \\ y_m \\ 1 \end{pmatrix}$$

$m_{22}$  set to 1.

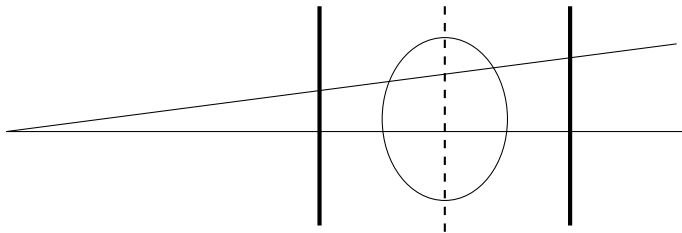
8 remaining parameters to find.

## IDEAL AND MEASURED POINTS



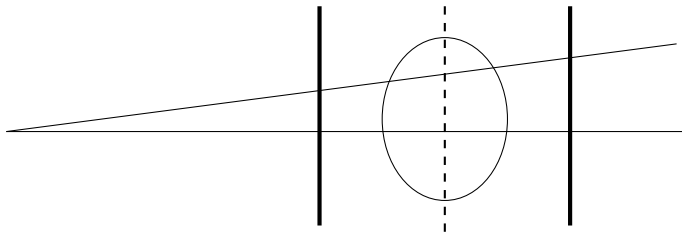
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- Accelerator plan spot position on isocenter plane projected to ideal detector plane

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- Accelerator plan spot position on isocenter plane projected to ideal detector plane
- Mean of measured hits of spot as measured point



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- Points well spread. Spot separation and domain coverage.
- Sensitive to noise.
- Go to overdetermined system

# SOLVING FOR $M$

Solve using non-linear optimization (modified Levenberg-Marquardt).

Given  $k$  measured points  $p_m$  and their corresponding ideal representations  $(p_m, p_i)$  point pairs, create  $2k$  expressions to minimize,

$$\frac{x(Mp_{m_j})}{w(Mp_{m_j})} - x_{i_j}$$

$$\frac{y(Mp_{m_j})}{w(Mp_{m_j})} - y_{i_j}$$

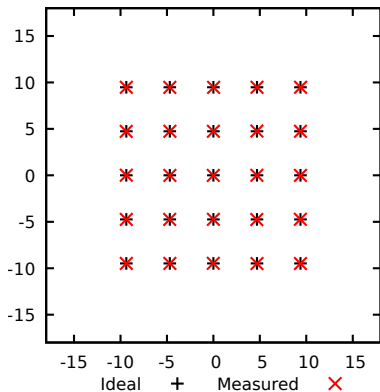
or

$$\frac{m_{00}x_{m_j} + m_{01}y_{m_j} + m_{02}}{m_{20}x_{m_j} + m_{21}y_{m_j} + 1} - x_{i_j}$$

$$\frac{m_{10}x_{m_j} + m_{11}y_{m_j} + m_{12}}{m_{20}x_{m_j} + m_{21}y_{m_j} + 1} - y_{i_j}$$

# UPSTREAM DETECTOR — BASE CASE

Upstream Measured Points vs Ideal Points

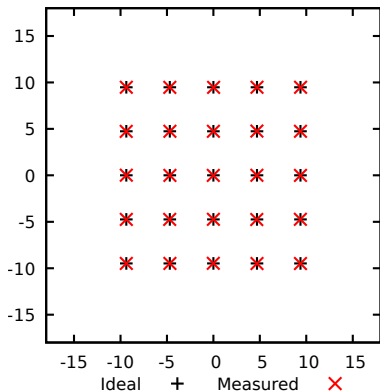


Computed:

$$\begin{pmatrix} 0.999906 & -0.00058756 & 0.003631 \\ -0.0002755 & 0.999784 & 0.0005824 \\ 4.8408E-05 & 1.3831E-06 & 1.0 \end{pmatrix}$$

# UPSTREAM DETECTOR — BASE CASE

Upstream Measured Points vs Ideal Points



Ideal:

$$\begin{pmatrix} 1.00000 & 0.00000 & 0.0 \\ 0.00000 & 1.00000 & 0.0 \\ 0.00000 & 0.00000 & 1.0 \end{pmatrix}$$

Computed:

$$\begin{pmatrix} 0.999906 & -0.00058756 & 0.003631 \\ -0.0002755 & 0.999784 & 0.0005824 \\ 4.8408E-05 & 1.3831E-06 & 1.0 \end{pmatrix}$$

# UPSTREAM DETECTOR — BASE CASE



Figure: Uncorrected

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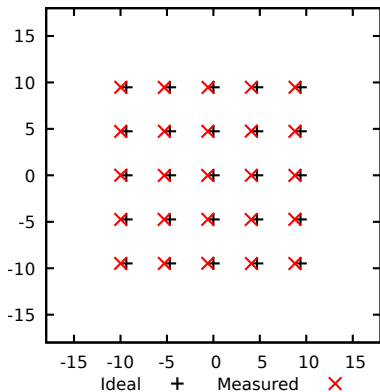


Figure: Corrected



# UPSTREAM DETECTOR — 6MM TRANSVERSE TRANSLATION

Upstream Measured Points vs Ideal Points

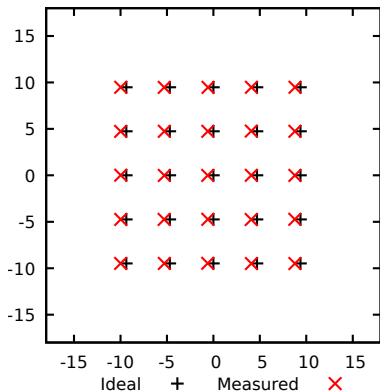


Computed:

$$\begin{pmatrix} 0.999877 & -0.00058758 & 0.603557 \\ -0.00027545 & 0.999755 & 0.0004168 \\ 4.8403E-05 & 1.3714E-06 & 1.0 \end{pmatrix}$$

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Ideal:

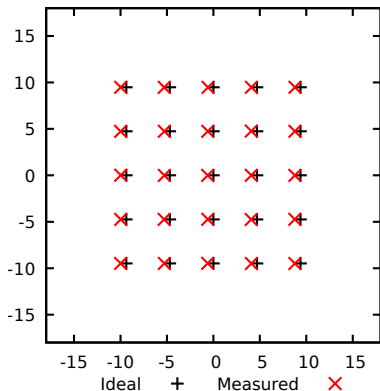
$$\begin{pmatrix} 1.0000000 & 0.0000000 & T_x \\ 0.0000000 & 1.0000000 & T_y \\ 0.0000000 & 0.0000000 & 1.0 \end{pmatrix}$$

Computed:

$$\begin{pmatrix} 0.999877 & -0.00058758 & 0.603557 \\ -0.00027545 & 0.999755 & 0.0004168 \\ 4.8403E-05 & 1.3714E-06 & 1.0 \end{pmatrix}$$

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$$T_1 = 6.03557 \text{ mm,}$$

$$T_2 = 0.603557/0.999877 = 6.03631 \text{ mm}$$

# UPSTREAM DETECTOR — 6MM TRANSVERSE TRANSLATION



Figure: Uncorrected

# UPSTREAM DETECTOR — 6MM TRANSVERSE TRANSLATION



Figure: Corrected

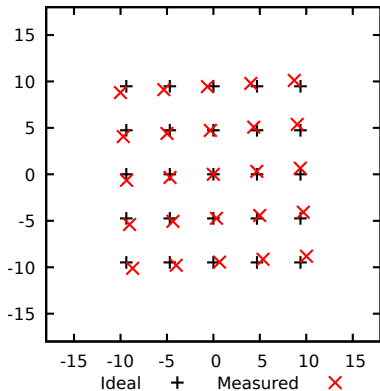
# UPSTREAM DETECTOR — 6MM TRANSVERSE TRANSLATION



Figure: Baseline

# UPSTREAM DETECTOR — 4° AXIAL ROTATION

Upstream Measured Points vs Ideal Points

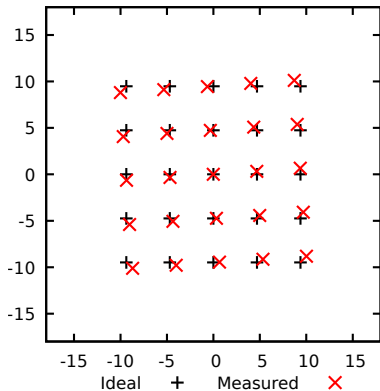


Computed:

$$\begin{pmatrix} 0.997589 & 0.069128 & 0.003283 \\ -0.069904 & 0.997270 & 0.003206 \\ 0.000050 & 0.000030 & 1.0 \end{pmatrix}$$

# UPSTREAM DETECTOR — 4° AXIAL ROTATION

Upstream Measured Points vs Ideal Points



Ideal:

$$\begin{pmatrix} \cos \theta & -\sin \theta & 0.0 \\ \sin \theta & \cos \theta & 0.0 \\ 0.0 & 0.0 & 1.0 \end{pmatrix}$$

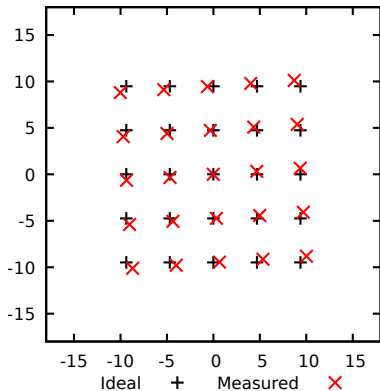
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Upstream Measured Points vs Ideal Points



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Computed:

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$$R_1 = \cos^{-1}(0.997589) \Rightarrow \theta = \pm 3.979^\circ$$

$$R_2 = \cos^{-1}(0.997270) \Rightarrow \theta = \pm 4.234^\circ$$

$$R_3 = \sin^{-1}(-0.069904) \Rightarrow \theta = -4.008^\circ$$

$$R_4 = \sin^{-1}(-0.069128) \Rightarrow \theta = -3.964^\circ$$

# UPSTREAM DETECTOR — 4° AXIAL ROTATION



Figure: Uncorrected

# UPSTREAM DETECTOR — 4 DEG AXIAL ROTATION

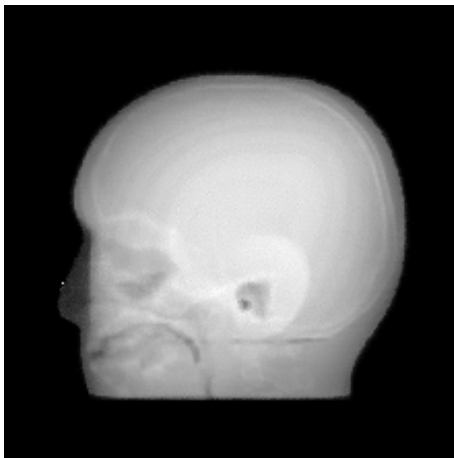


Figure: Corrected

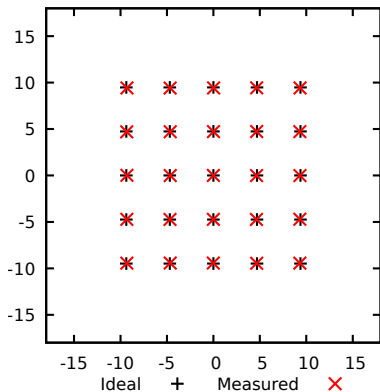
# UPSTREAM DETECTOR — 4 DEG AXIAL ROTATION



Figure: Baseline

# UPSTREAM DETECTOR — 12MM AXIAL TRANSLATION

Upstream Measured Points vs Ideal Points

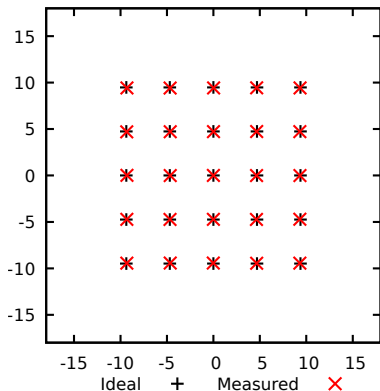


Computed:

$$\begin{pmatrix} 1.006587 & -0.000506 & 0.003253 \\ -0.000133 & 1.005249 & 0.003159 \\ 0.000051 & 0.000018 & 1.0 \end{pmatrix}$$

# UPSTREAM DETECTOR — 12MM AXIAL TRANSLATION

Upstream Measured Points vs Ideal Points



$$S'_x = S_x + z_u - dz_u/2$$

$$S'_y = S_y + z_u + dz_u/2$$

$$k_x = S'_x / (S'_x + \Delta z)$$

$$k_y = S'_y / (S'_y + \Delta z)$$

Ideal:

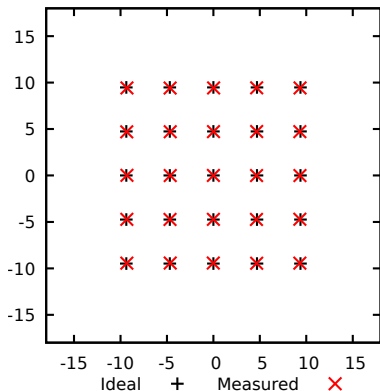
$$\begin{pmatrix} k_x & 0 & 0 \\ 0 & k_y & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Computed:

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# UPSTREAM DETECTOR — 12MM AXIAL TRANSLATION

Upstream Measured Points vs Ideal Points



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$$S'_y = S_y + z_u + dz_u/2$$

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$$k_y = S'_y / (S'_y + \Delta z)$$

Ideal:

$$\begin{pmatrix} k_x & 0 & 0 \\ 0 & k_y & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Computed:

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$$k_x \Rightarrow \Delta z = -11.871 \text{ mm}$$

$$k_y \Rightarrow \Delta z = -11.404 \text{ mm}$$

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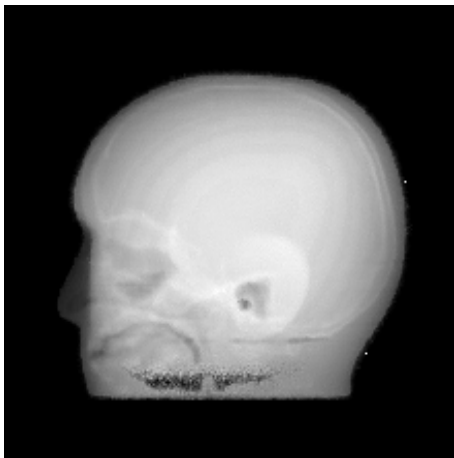


Figure: Uncorrected



# UPSTREAM DETECTOR — 12MM AXIAL TRANSLATION



Figure: Corrected

# UPSTREAM DETECTOR — 12MM AXIAL TRANSLATION



Figure: Baseline



## CONCLUSION AND FUTURE WORK

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- Feasible detector alignment correction



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- Feasible detector alignment correction
- Alignment using image data instead of alignment scan

## ACKNOWLEDGEMENTS

- NIU Computer Science Department
  - Nicholas Karonis, Cesar Ordoñez, John Winans
- NIU Physics Department
  - George Coutrakon
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- Northwestern Medicine Proton Center
  - James Welsh, Mark Pankuch