



Ion imaging with a time-of-flight ion computed tomography system based on ultra-fast silicon sensors

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at GSI and the ion CT group of HEPHY and TU WIEN**

Ultra Fast Silicon Detectors/Low Gain Avalanche Diodes

Low Gain Avalanche Diodes (LGADs)

- thin silicon detector optimized for timing performance
 - gain layer exhibits high electric fields ($> 300 \text{ keV/cm}$)
 - leads to intrinsic signal amplification
 - results in large signals with short rise times ($< 1 \text{ ns}$)

■ why low gain?

- high gain also amplifies noise
 - leads to temporal signal fluctuations (time jitter)
 - deteriorates time resolution
- LGADs are operated at controlled low gain ($\approx 10\text{-}30$)
 - to optimize SNR and time resolution

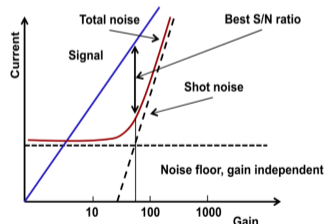
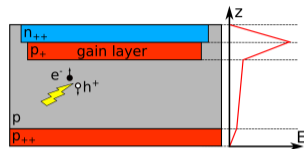
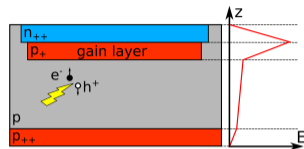


Figure: Sadrozinski et al. 2017

Low Gain Avalanche Diodes (LGADs)

- thin silicon detector optimized for timing performance
 - gain layer exhibits high electric fields (> 300 keV/cm)
 - leads to intrinsic signal amplification
 - results in large signals with short rise times (< 1 ns)

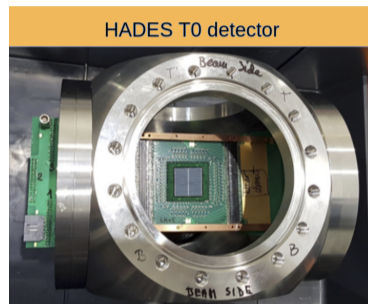


- why low gain?
 - high gain also amplifies noise
 - leads to temporal signal fluctuations (time jitter)
 - deteriorates time resolution
 - LGADs are operated at controlled low gain ($\approx 10-30$)
 - to optimize SNR and time resolution

$$\sigma_T^2 \approx \underbrace{\left(\frac{T_{\text{rise}}}{\text{SNR}} \right)^2}_{\sigma_{\text{jitter}}^2} + \underbrace{\sigma_{T,\text{floor}}^2}_{\text{gain indep.}}$$

Low Gain Avalanche Diodes (LGADs)

- LGADs are promising candidates for 4D-tracking
 - time resolutions down to **30-50 ps** possible
 - high spatial resolution ($< 100 \mu\text{m}$)
 - low material budget ($X/X_0 \ll 1 \%$)
 - radiation hard ($\approx 10^{15} n_{\text{eq}}/\text{cm}^2$)
 - large sensor areas $\mathcal{O}(\text{cm}^2)$
 - high particle rates (e.g. 10^8 p/s/cm^2 at HADES)
- high interest in high energy physics community
 - CERN high luminosity upgrade
 - ATLAS High-Granularity Timing Detector (HGTD)
 - CMS Endcap Timing Layer (ETL)
 - HADES T0 detector at GSI
 - beam monitor system at S-DALINAC
 - radiation detector for space applications

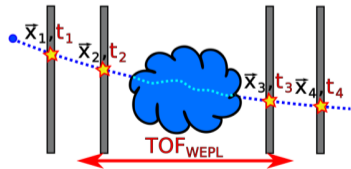
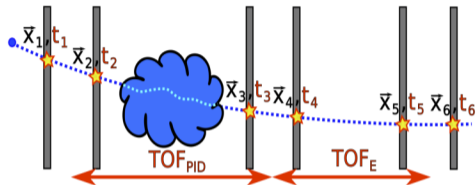


- but also medical applications
 - ion therapy beam quality monitor ([Vignati et al. 2023](#))
 - **ion imaging**

LGAD-based TOF-iCT system

- LGAD-based TOF-iCT system
 - requires 6 4D-tracking layers
 - TOF in air for residual energy determination
 - TOF through object + energy loss for PID ([Rovituso et al. 2017](#))

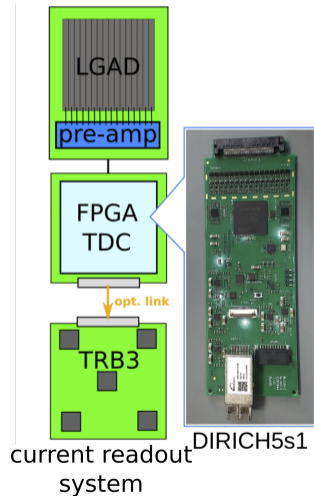
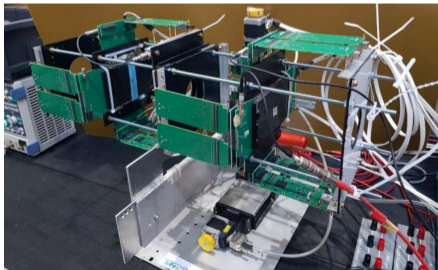
- second approach: “sandwich” TOF-iCT
 - indirect WEPL measurement via TOF through object ([Ulrich-Pur 2022](#))
 - no need for residual energy detector
 - requires only 4 4D-tracking layers
 - compact scanner design



TOF-iCT demonstrator system

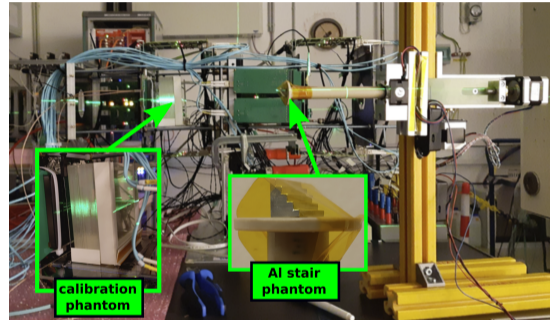
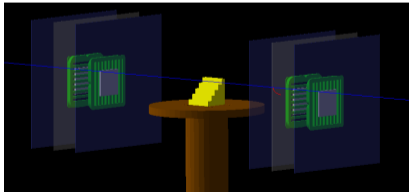
TOF-iCT demonstrator - current setup

- TOF-iCT demonstrator at GSI
 - four $1 \times 1 \text{ cm}^2$ FBK strip LGADs with $100 \mu\text{m}$ pitch
 - discrete front-end electronics
 - FPGA-based TDCs with leading-edge discriminator
 - 4x DIRICH5s1 (32 channels per DiRICH)
 - imaging of small objects $\mathcal{O}(< 1 \text{ cm}^2)$



TOF-iCT demonstrator - first experiment

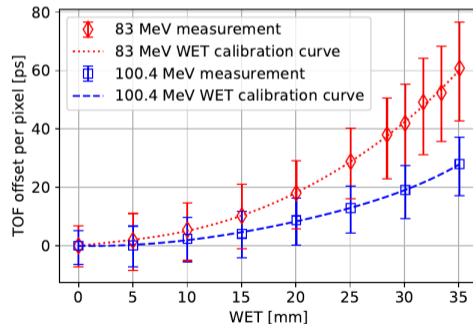
- MedAustron testbeam in April 2023
 - 10^5 p/s protons with 83 and 100.4 MeV
 - 1.6 mm PMMA slabs for WEPL calibration
 - pRad of Al stair phantom was recorded



- first experimental TOF-based (Sandwich) pRad: [Ulrich-Pur et al. 2024](#)

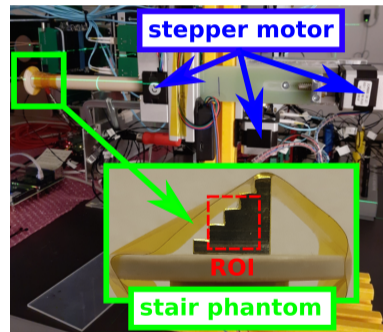
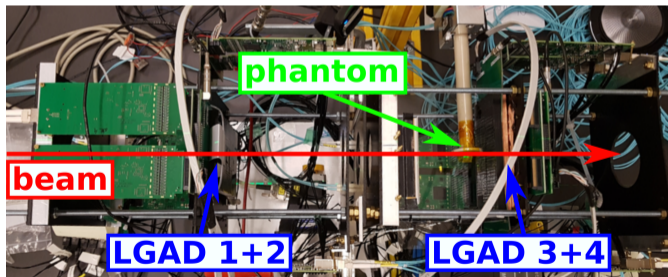
TOF-iCT demonstrator - WET calibration

- TOF per pixel was measured for different PMMA absorber thicknesses at two different beam energies
- 5th-order polynomial was used to fit the increase in TOF to the corresponding WET

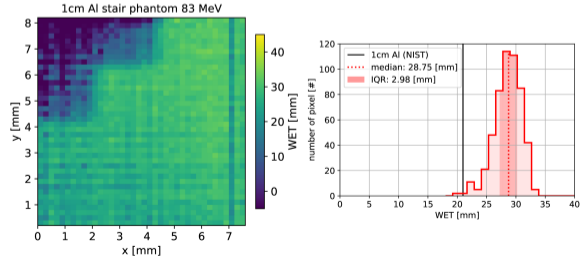
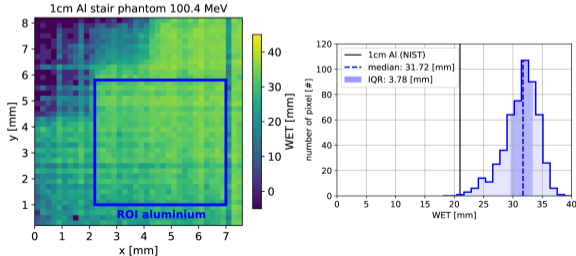


TOF-iCT demonstrator - Sandwich TOF-pRad

- All stair phantom was mounted on rotational table
 - due to alignment and size of sensors, only part of phantom could be imaged (ROI)
- pRads were recorded at 83 and 100.4 MeV

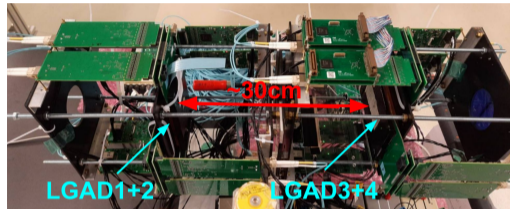


- increase in TOF was measured in $0.2 \times 0.2 \text{ mm}^2$ pixels projected onto the last two LGAD planes (i.e. 2×2 LGAD strips per pixel)
 - on last LGAD, only every second channel was connected
- Al stair phantom still clearly visible
 - however, WET overestimated
 - upgrade of setup and improvement of systematic errors is ongoing



TOF-iCT demonstrator - TOF calorimeter

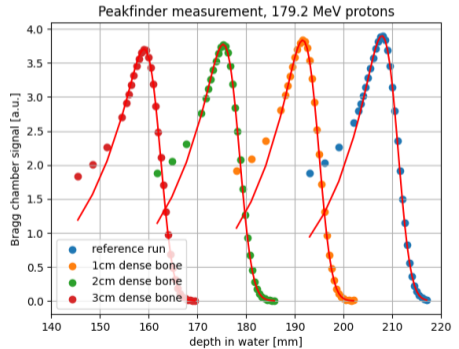
- second testbeam in June 24
 - TOF-iCT demonstrator operated as TOF calorimeter
 - TOF in air was correlated to beam energy
 - WET measurements were performed
 - different particle rates were tested



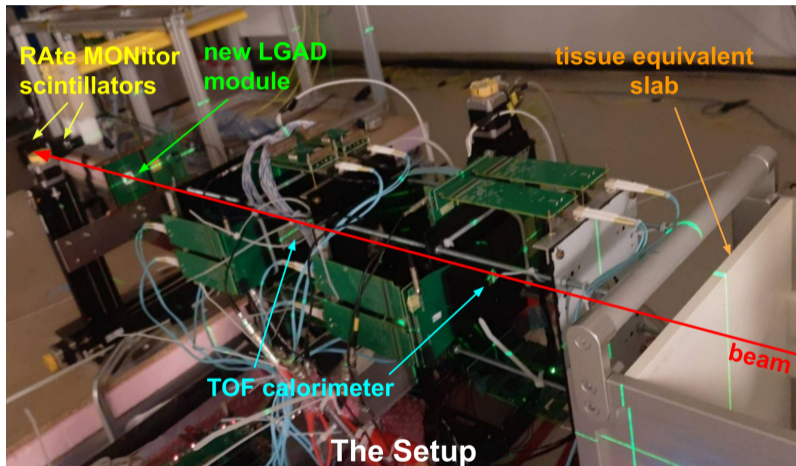
- small changes were made to the TOF-iCT demonstrator
 - added new FPGA TDCs to fully read out all sensors
 - scanner length was increased to 30 cm

TOF-iCT demonstrator - TOF calorimeter

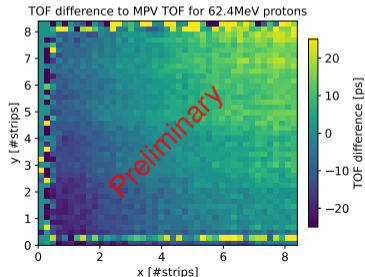
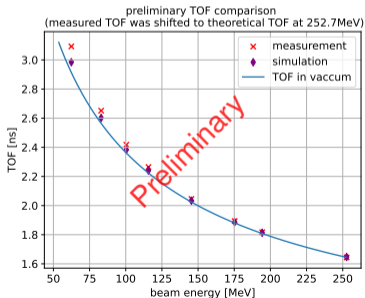
- 1 cm thick CIRS slabs
 - solid water and dense bone were used
 - RSP reference was measured with the PTW Peakfinder



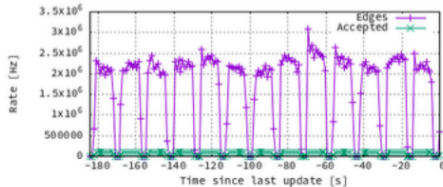
TOF-iCT demonstrator - TOF calorimeter



- energy vs TOF calibration was done prior to WET measurements
 - TOF was determined for beam energies between 62.4 MeV and 252.7 MeV
 - measurements were compared to simulation and TOF in vacuum
- still, systematic errors visible
 - possible tilt of LGADs detected
 - TOF distribution could be used for track-based alignment procedure (WIP)

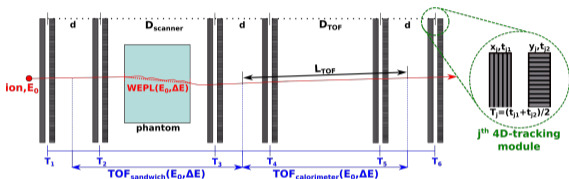


- WET accuracy optimization still WIP
- but what about speed?
 - during HADES experiment at GSI 10^8 p/s/cm² rising edges were detected
 - at MedAustron, on the other hand, a reduced particle rate was used to provide clean 4D particle tracks $\mathcal{O}(100$ kHz) – $\mathcal{O}(4$ MHz) rates)
 - particle rate measured with scintillators matched rates on LGADs
 - however, current DAQ is limited by 100 kHz
- upgraded DAQ is already developed and being tested (DOGMA system)

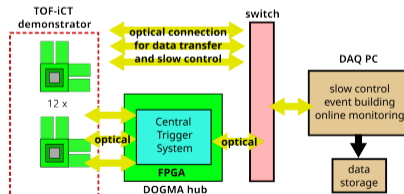
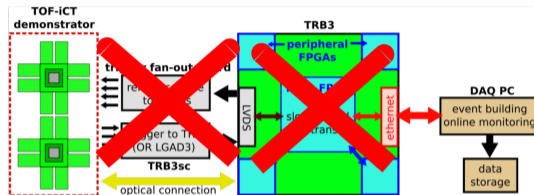


Future and current upgrades for the TOF-iCT demonstrator system

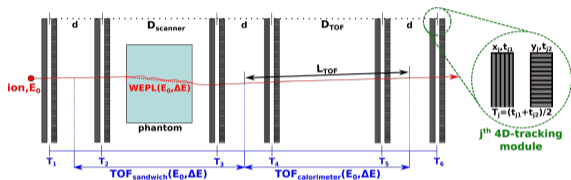
Next version of the ion imaging demonstrator



- small, but full TOF-iCT system
 - 12 single-sided LGAD strip sensors with upgraded front-end-electronics
 - DOGMA readout system with optical data transfer



Next version of the ion imaging demonstrator



- small, but full TOF-iCT system
 - 12 single-sided LGAD strip sensors with upgraded front-end-electronics
 - DOGMA readout system with optical data transfer

- development and testing of next scanner is part of FWF Erwin Schrödinger grant Nr J 4762-N
 - first 4D-tracking module will be tested soon at MedAustron
 - both Sandwich TOF-iCT and standard TOF-iCT will be investigated with new scanner
 - data sets for Sandwich TOF-iCT will be created

Summary and outlook

- LGADs are promising 4D-tracking detectors with many applications
 - well-suited for ion imaging
- two different scanner concepts
 - “standard” TOF-iCT system with a TOF calorimeter
 - sandwich TOF-iCT system without a residual energy detector
- TOF-iCT demonstrator system
 - demonstrator system based on LGAD strip sensors was built and tested
 - first sandwich TOF-pRad of an aluminium stair phantom was successfully recorded at MedAustron to show proof-of-principle
 - WET measurements with TOF calorimeter were performed
 - systematics of real experiment are being studied

- Sandwich TOF-iCT
 - WEPL calibration algorithms will be further optimized
 - semi-analytical approach in development (Stephan Kwas)
 - STOFICT project by CREATIS recently received funding (Simon Rit et al.)
- short-term goal
 - improvement of current demonstrator system
 - further measurements with demonstrator system planned
- future large-area system
 - requires dedicated ASIC which can handle high rates and large number of channels
 - dedicated module design to build low-mass large area system

Thank you for your attention!

■ TU WIEN/HEPHY

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- Andreas Gsponer
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- Matthias Kausel
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- Daniel Makay
- Stephan Kwas

■ GSI

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- Michael Traxler

■ FBK

■ CREATIS

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Backup

Community Input for NuPECC Long Range Plan 2024

Ultra-fast silicon detectors for nuclear physics and medical applications

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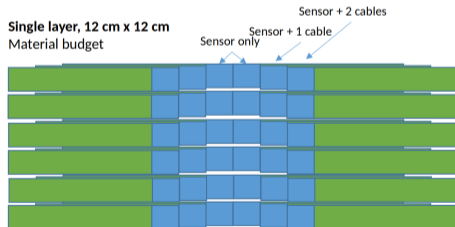
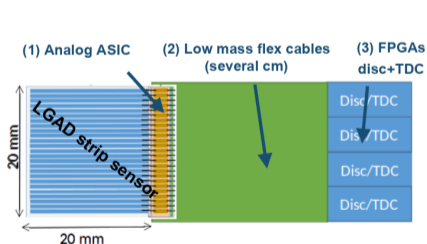
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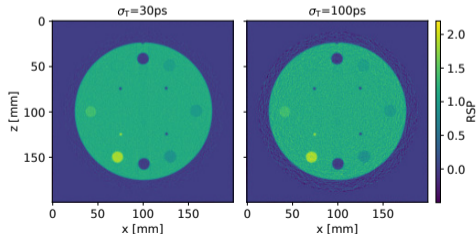
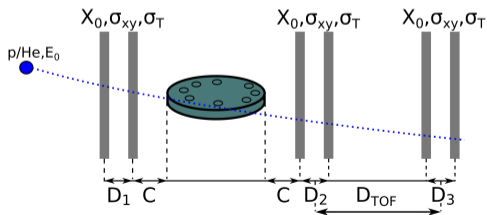
Future large-area 4D-tracking system

- novel LGAD sensors with increased fill factor will be investigated
 - new sensor production with trench-isolated LGADs planned
- upgraded readout electronics with increased number of readout channels
 - dedicated ASIC and FPGA-based TDCs
- dedicated low-mass module design for large active areas (tens of cm^2)
 - low mass flex cables to reduce overall material budget ($X/X_0 < 1\%$)



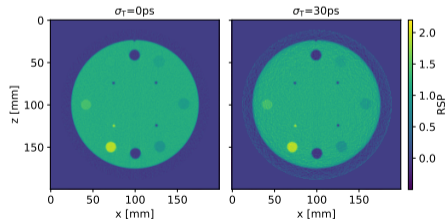
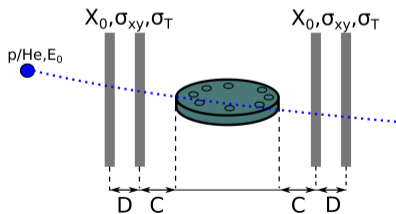
LGAD-based TOF-iCT system - previous work

- Monte Carlo feasibility study ([Ulrich-Pur et al. 2022](#))
 - realistic model of LGAD-based TOF-iCT system
 - assessment of image quality using the CTP404 phantom
 - study of RSP accuracy and resolution
 - RSP MAPE down to **0.12%**
 - time resolution \leq **30-50 ps** required
 - see also [Krah et al. 2022](#)

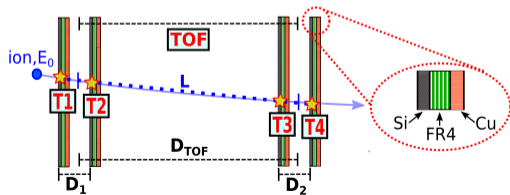


“Sandwich” TOF-iCT - previous work

- Monte Carlo feasibility study ([Ulrich-Pur et al. 2023](#))
 - same MC model as in “standard” TOF-iCT study
 - determine influence of different system parameters on image quality
 - influence on RSP accuracy and resolution
 - measured with CTP 404 phantom
 - first study based on simple WEPL calibration approach to show proof-of-principle
 - WEPL estimation needs still further optimization
 - semi-analytical method currently under investigation



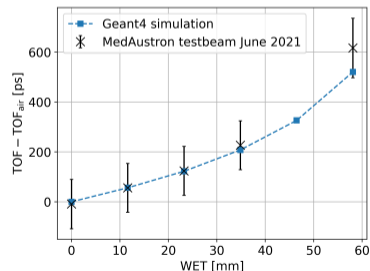
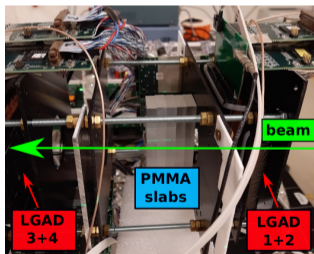
- Monte Carlo feasibility studies (Ulrich-Pur et al. 2022)
 - see LLU workshop 2021
 - performance study of stand-alone TOF calorimeter
 - influence of system parameters on energy resolution and accuracy
 - implementation of dedicated calibration procedure
 - time resolution 30-50 ps required
 - energy modulation, length of the calorimeter and number of LGADs can be adjusted to optimize the time resolution



$$E_{\text{kin}} = m_0 c^2 \left(\frac{1}{\sqrt{1 - \frac{L^2}{c^2} \text{TOF}^2 - 1}} \right)$$

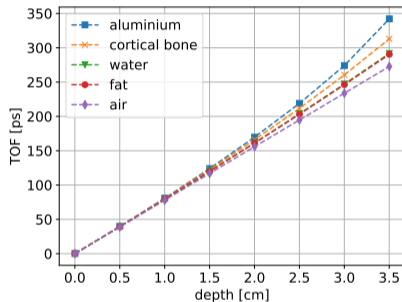
“Sandwich” TOF-iCT - previous work

- first proof-of-principle measurement at MedAustron in 2021 (Krüger et al. 2022)
 - 4 LGAD strip sensors (HADES) with different geometries
 - total active area: $0.5 \times 0.5 \text{ cm}^2$
 - 100.4 MeV protons with $\approx 5 \times 10^6 \text{ p/s}$
 - increase in TOF for different PMMA absorbers



“Sandwich” TOF-iCT - motivation

- main idea:
 - particles loose energy along their path
 - TOF increases depending on traversed material and beam energy
 - find method to exploit increase in TOF through object for WEPL estimation
 - define “new” material dependent quantity, i.e. slowing down power (SDP)
 - define imaging problem
 - find method to map the SDP to the stopping power (SP)



$$\text{TOF} = \int_0^L \frac{ds}{v(\vec{x}(s))} \neq \frac{L}{v}$$

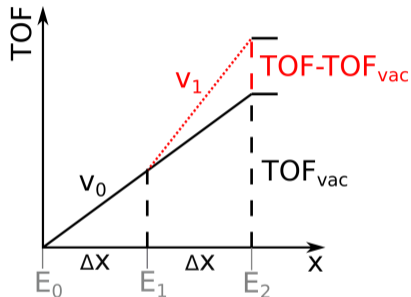
“Sandwich” TOF-iCT - concept

- definition of “slowing down power”
 - increase in TOF with respect to the TOF in vacuum per unit path length

$$\text{SDP}(E_{\text{kin}}(\vec{x}(s))) := \frac{\text{TOF} - \text{TOF}_{\text{vac}}}{\Delta s}(E_{\text{kin}}(\vec{x}(s)))$$

- SDP is directly related to SP

$$\text{SDP}(E(x)) \approx -\frac{\Delta x}{2v^2(E(x))} v'(E(x)) \cdot \text{SP}(E(x))$$



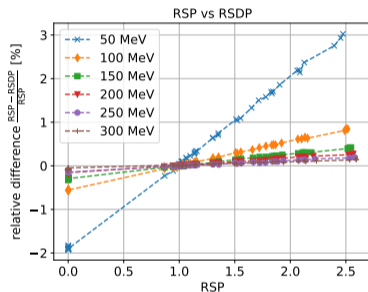
“Sandwich” TOF-iCT - concept

- define relative slowing down power (RSDP)
 - RSDP is approximately equal to the RSP
 - WEPL definition stays the same

$$\text{RSDP} := \frac{\text{SDP}_{\text{mat}}(E(x))}{\text{SDP}_{\text{H}_2\text{O}}(E(x))} \approx \text{RSP}$$

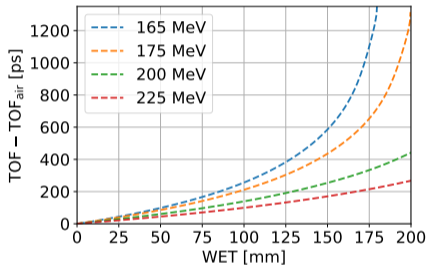
- inverse problem

$$\text{WEPL} := \int_0^{\text{TOF} - \text{TOF}_{\text{vac}}} \frac{d\Delta\text{TOF}}{\text{SDP}_{\text{H}_2\text{O}}(\Delta\text{TOF}(E(\vec{x}(s))))} = \int_0^L \text{RSDP}(\vec{x}(s)) ds \approx \int_0^L \text{RSP}(\vec{x}(s)) ds$$



“Sandwich” TOF-iCT - concept

- measuring increase in TOF w.r.t vacuum is challenging
 - requires accurate velocity map to determine TOF in vacuum
 - can be obtained e.g. via MC simulations
- simpler approach
 - measure TOF increase w.r.t TOF in air and calibrate against WEPL
 - use e.g. 5th-order polynomial for calibration



$$TOF - TOF_{air}(WEPL, E_0) \approx \sum_{i=0}^5 a_i(E_0) \cdot WEPL^i$$

TOF in matter

$$\text{TOF} = \int_0^L \frac{ds}{v(\mathbf{x}(s))} = \int_0^L \frac{ds}{c \frac{E_{\text{kin}}(\mathbf{x}(s))}{E_{\text{kin}}(\mathbf{x}(s)) + m_0 c^2} \sqrt{1 + 2 \frac{m_0 c^2}{E_{\text{kin}}(\mathbf{x}(s))}}}$$

- depends on traversed material and beam energy

Increase in TOF

$$\Delta\text{TOF} = \text{TOF} - \text{TOF}_{\text{vac}} = \int_0^{\Delta x} \frac{ds}{v(\mathbf{x}(s))} - \frac{\Delta x}{v(\mathbf{x}(s=0))}$$

- define slowing down power to describe the material dependent increase in TOF

TOF in matter for $L = 2\Delta x$

$$\text{TOF} = \frac{\Delta x}{v(E(x))} + \frac{\Delta x}{v(E(x+\Delta x))}$$

1st-order Taylor expansion

$$\text{TOF} \approx \frac{2\Delta x}{v(E(x))} - \frac{\Delta x^2}{v^2(E(x))} \frac{\partial v(E(x))}{\partial x}$$

TOF in vacuum

$$\text{TOF}_{\text{vac}} = \frac{2\Delta x}{v(E(x))}$$

increase in TOF

$$\text{TOF} - \text{TOF}_{\text{vac}} \approx -\frac{\Delta x^2}{v^2(E(x))} \frac{\partial v(E(x))}{\partial x}$$

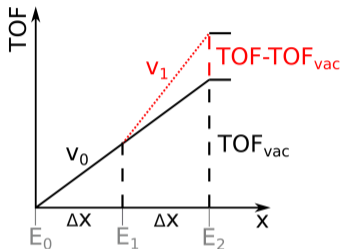


Figure: SDP definition

Slowing down power

$$\text{SDP}(E_{\text{kin}}(\mathbf{x}(s))) := \frac{\text{TOF} - \text{TOF}_{\text{vac}}}{\Delta s}(E_{\text{kin}}(\mathbf{x}(s)))$$

SDP for $L = 2\Delta x$

$$\text{SDP}(E(x)) = \frac{\text{TOF} - \text{TOF}_{\text{vac}}}{2\Delta x} \approx -\frac{\Delta x}{2v^2(E(x))} \frac{\partial v(E(x))}{\partial x}$$

approximation of derivative

$$\frac{\partial v(E(x))}{\partial x} = \frac{\partial v(E(x))}{\partial E(x)} \frac{\partial E(x)}{\partial x} \approx v'(E(x)) \cdot \text{SP}(E(x))$$

using

$$\frac{\partial E(x)}{\partial x} \approx \text{SP}(E(x)) \text{ and } v'(E(x)) = \frac{\partial v(E(x))}{\partial E(x)}$$

relation SDP and SP

$$\text{SDP}(E(x)) \approx -\frac{\Delta x}{2v^2(E(x))} v'(E(x)) \cdot \text{SP}(E(x))$$

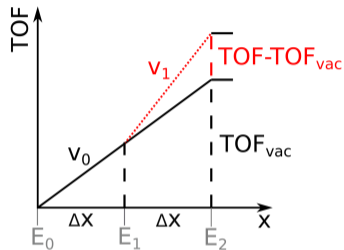


Figure: SDP definition

Slowing down power

$$\text{SDP}(E_{\text{kin}}(\mathbf{x}(s))) := \frac{\text{TOF} - \text{TOF}_{\text{vac}}}{\Delta s}(E_{\text{kin}}(\mathbf{x}(s)))$$

Relative slowing down power (RSDP)

$$\text{RSDP} := \frac{\text{SDP}_{\text{mat}}(E(x))}{\text{SDP}_{\text{H}_2\text{O}}(E(x))}$$

RSDP vs RSP

$$\text{RSDP} \approx \frac{-\frac{\Delta x}{2v^2(E(x))} v'(E(x)) \cdot \text{SP}_{\text{mat}}(E(x))}{-\frac{\Delta x}{2v^2(E(x))} v'(E(x)) \cdot \text{SP}_{\text{H}_2\text{O}}(E(x))} = \text{RSP}$$

- RSDP is approximately equal to RSP
- WEPL definition is also the same

WEPL

$$\text{WEPL} = \int_0^L \text{RSP}(\mathbf{x}(s)) ds \approx \int_0^L \text{RSDP}(\mathbf{x}(s)) ds$$

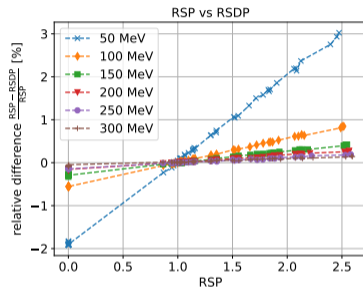


Figure: RSP error

RSDP vs RSP

$$\text{RSDP} := \frac{\text{SDP}_{\text{mat}}(E(x))}{\text{SDP}_{\text{H}_2\text{O}}(E(x))} \approx \text{RSP}$$

Imaging problem

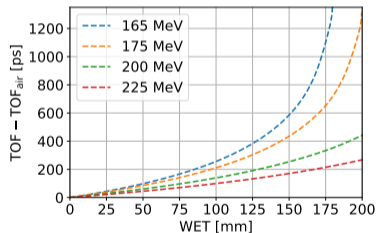
$$\text{WEPL} := \int_0^{\text{TOF} - \text{TOF}_{\text{vac}}} \frac{d\Delta\text{TOF}}{\text{SDP}_{\text{H}_2\text{O}}(\Delta\text{TOF}(E(\mathbf{x}(s))))} = \int_0^L \text{RSDP}(\mathbf{x}(s)) ds \approx \int_0^L \text{RSP}(\mathbf{x}(s)) ds$$

Measuring increase in TOF w.r.t vacuum is challenging

- requires accurate velocity map to determine TOF in vacuum
 - can be obtained e.g. via MC simulations

Simpler approach

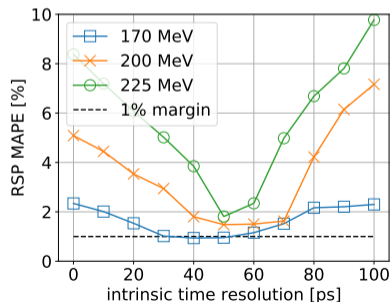
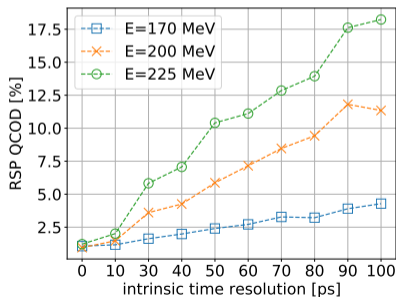
- measure TOF increase w.r.t TOF in air and calibrate against WEPL
 - use e.g. 5th-order polynomial for calibration



$$\text{TOF} - \text{TOF}_{\text{air}}(\text{WEPL}, E_0) \approx \sum_{i=0}^5 a_i(E_0) \cdot \text{WEPL}^i$$

“Sandwich” TOF-iCT - MC study

- RSP resolution (QCOD) shows similar dependence on time resolution and beam energy when compared to standard TOF-iCT system
- RSP accuracy $\geq 0.91\%$
 - still shows systematic dependence on system parameters
 - more dedicated calibration procedure/model is currently under investigation



explanation of u-shape of MAPE

- RSP is generally overestimated (positive RSP error)
 - skewed TOF distribution results in shift towards higher TOF and therefore WET values
 - caused by non-straight paths (MCS) etc.
- intrinsic time resolution compensates for this effect
 - time measurement error results in asymmetric shift on WET distribution (last slide)
 - shifted towards lower WET values
 - RSP error decreases and becomes negative

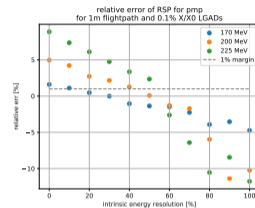


Figure: rel. err in PMP

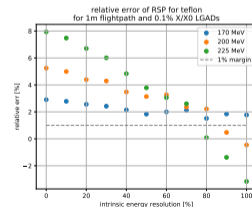
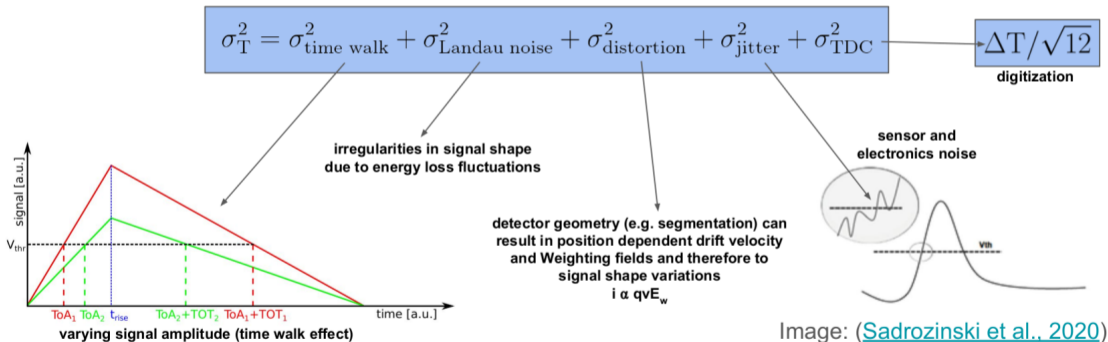
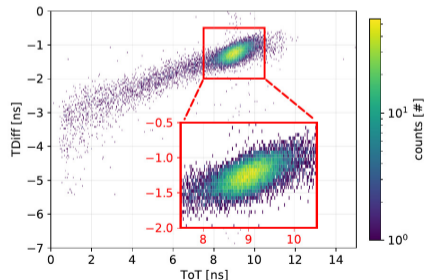
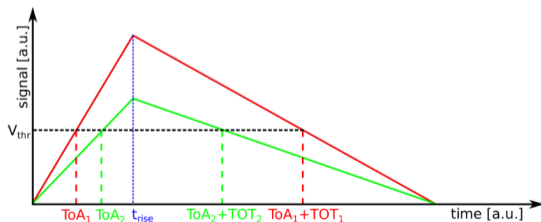


Figure: rel. err in Teflon

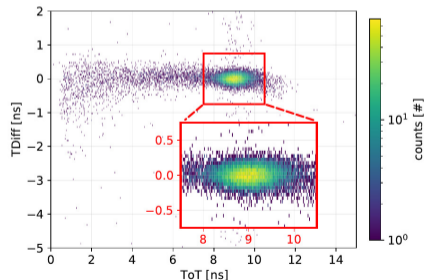
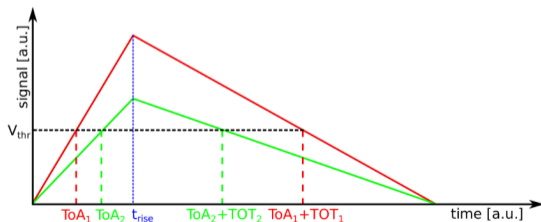
- final time resolution depends on every step in the readout chain



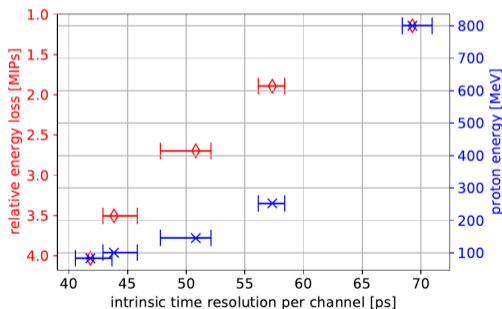
- precise time measurements require precise sensor calibration
 - calibration of constant threshold signal discrimination (time-walk effect)
 - synchronisation of all LGAD channels per 4D-tracking module (offset correction)
- time-walk and offset correction was performed for each LGAD channel



- precise time measurements require precise sensor calibration
 - calibration of constant threshold signal discrimination (time-walk effect)
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- time-walk and offset correction was performed for each LGAD channel



- TOF and intrinsic time resolution was measured for different beam energies and every LGAD channel
 - time resolution improves with lower beam energy due to higher signal in detector
 - needs to be considered in simulations



- LGADs for beam monitoring (Krüger et al. 2022)

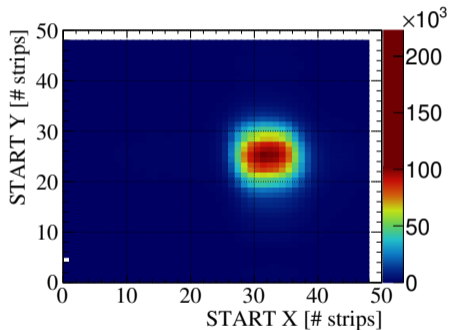


Figure: beam spot measurement

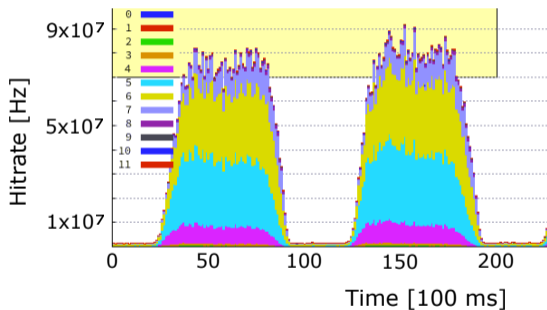
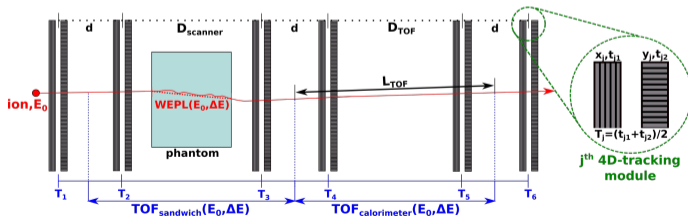






Figure: macro spill structure of p beam






TOF-iCT demonstrator - next steps

- current setup consists of only 2 4D-tracking layers
 - allows only straight-line approximation
- upgrade of current setup with more layers planned (Erwin-Schrödinger grant)
 - main goal: record first TOF-based iCT
 - additional 4D-tracking layers will allow implementation of MLP
 - more experimental data for TOF through matter will be recorded to further test and improve sandwich TOF-iCT models



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